

Notes for Assignment 2

Maths 323 fluids 2014

Last time:

Continuity Equation (Sec 6-7)

Force Balance (Sec 6-8)

Stream Function (Sec 6-9)

Postglacial Rebound (Sec 6-10)

Angle of Subduction (Sec. 6-11)

Diapirs intro (Sec 6-12)

Notes for Assignment 2

Maths 323 fluids 2014 Day 2

This time:

Diapirs (Sec 6-12)

Stokes Flow (Sec 6-14)

Equations so far

Continuity Equation in 2D

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \quad \text{where}$$

$$u = \frac{\partial x}{\partial t}; v = \frac{\partial y}{\partial t}$$

3-D: $\vec{\nabla} \cdot \vec{u} = 0$

Balance of pressure and viscous forces

Eq(6-67) $\frac{\partial P}{\partial x} = \mu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$

3-D: $\vec{\nabla} P = \mu \nabla^2 \vec{u}$

Eq(6-68) $\frac{\partial P}{\partial y} = \mu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)$

Where P=p-ρgy=deviatoric stress

$$u = -\frac{\partial \psi}{\partial y}; v = \frac{\partial \psi}{\partial x}$$

$$\nabla^4 \psi = 0$$

Stream function ψ
Biharmonic Equation:

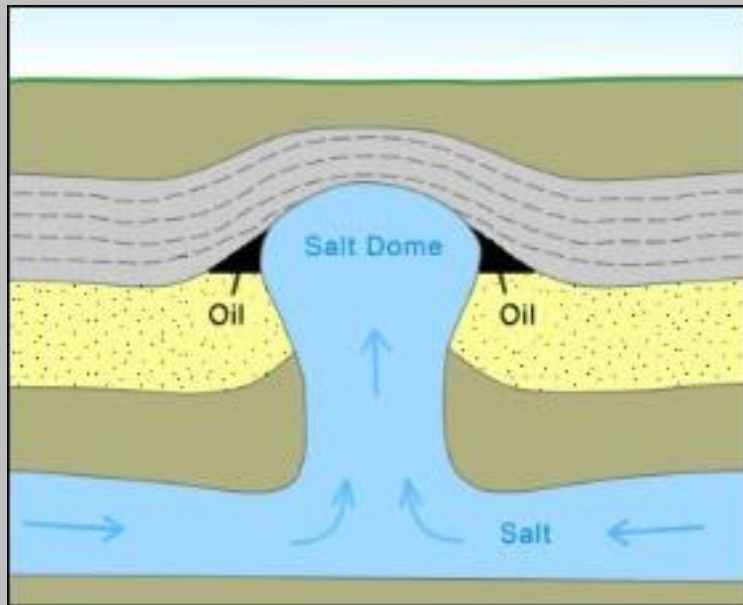
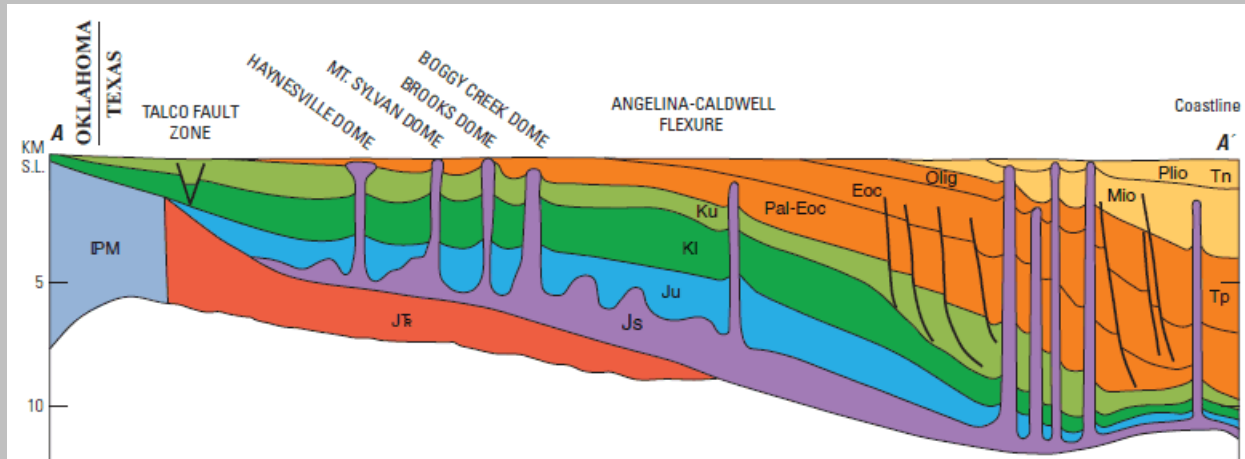
$$Q = \int_A^B d\psi = \psi_B - \psi_A$$

Flow rate from integral of stream function

Diapirs (Rayleigh-Taylor Instabilities) (not nappies)

- Driven by gravity and density imbalances—high over low
- Examples:
 - Paint dripping
 - Mantle “drips”
 - Start of convection, plumes, lava lamps
 - Salt domes
- Could grow exponentially until it breaks up, or could die out--returning to original state (but not periodic—not elastic)

Salt Domes



Images from :
<http://geology.com/stories/13/salt-domes/>

Basic Eqn: Incompressible continuity Eqn $\vec{\nabla} \cdot \vec{u} = 0$ or $\nabla^4 \psi = 0$

Balance Buoyancy Forces by Pressure Forces:

$$\vec{\nabla} P = \vec{\nabla} (p - \rho g y)$$

P=Pressure generated by fluid flow

p =pressure

Buoyancy= $\rho g y$

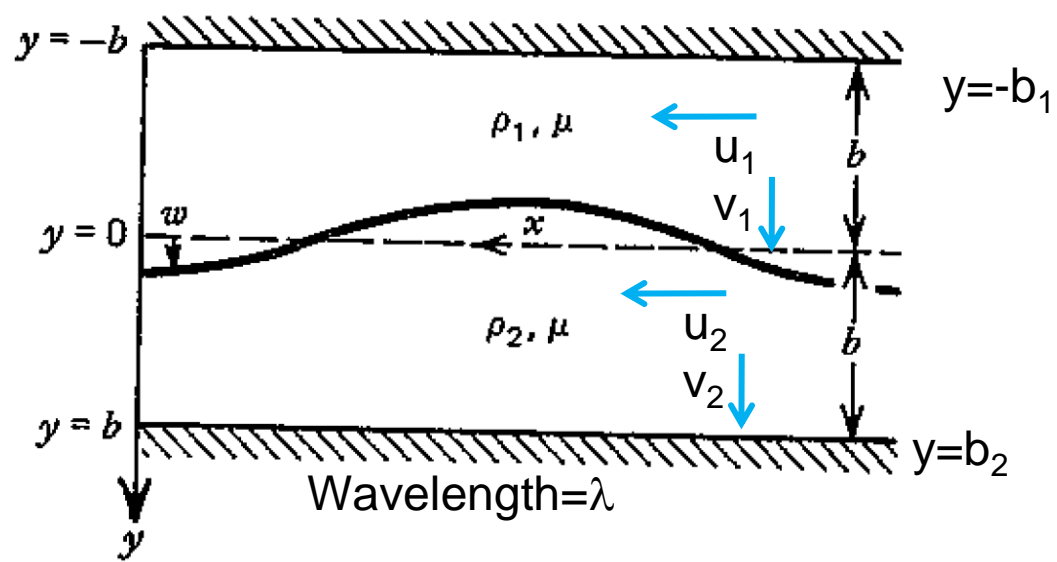
$$\vec{\nabla} P = \mu \nabla^2 u \quad (6-67 \text{ to } 6-68)$$

=0 if forces are in balance (e.g., eqn 6-151)

To solve eqn—introduce stream function ψ

Like postglacial rebound or subducting plate—but boundary conditions differ

6-21 The Rayleigh–Taylor instability of a dense fluid overlying a lighter fluid.



In general, $b_1 \neq b_2$

Displacement $w \ll b_1$ and b_2
 -- approximation is very important -- i.e.,
 Interface shape is
 $w = A \cos 2\pi x / \lambda$

Because A is small, can treat interface as if it were at $y=0$ for the purposes of solving boundary conditions

• **Boundary conditions:**

- 1) Rigid at top and bottom ($-b_1$ and b_2)—no slip condition (u continuous)
 $\therefore u=v=0$ at $y= -b_1$ and b_2
- 2) Displacements and velocities and shear stress must be continuous across boundary between media (i.e., at interface, but since w is small, effectively $y=0$ here)

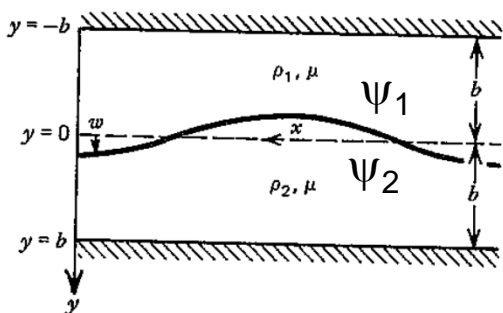
Guess solutions of ψ

- ψ_1 ; ψ_2 separate for each of top, bottom.
- ψ is similar in form to postglacial rebound, but uses hyperbolic functions instead of simple sines and cosines:

$$\sinh(x) = \frac{e^x - e^{-x}}{2}$$

$$\cosh(x) = \frac{e^x + e^{-x}}{2}$$

6-21 The Rayleigh-Taylor instability of a dense fluid overlying a lighter fluid.



$$\psi_1 = \sin \frac{2\pi x}{\lambda} \left(A_1 \cosh \frac{2\pi y}{\lambda} + B_1 \sinh \frac{2\pi y}{\lambda} + C_1 y \cosh \frac{2\pi y}{\lambda} + D_1 y \sinh \frac{2\pi y}{\lambda} \right) \quad (6-125)$$

(similar expression for ψ_2)

Solve by:

- Show that both $\psi_{1,2}$ are solns by substituting back into eqn,
- Determine $u_{1,2}$ and $v_{1,2}$ from derivatives of

- $\Psi_{1,2}$
$$u_{1,2} = -\frac{\partial \psi_{1,2}}{\partial y}; v_{1,2} = \frac{\partial \psi_{1,2}}{\partial x}$$

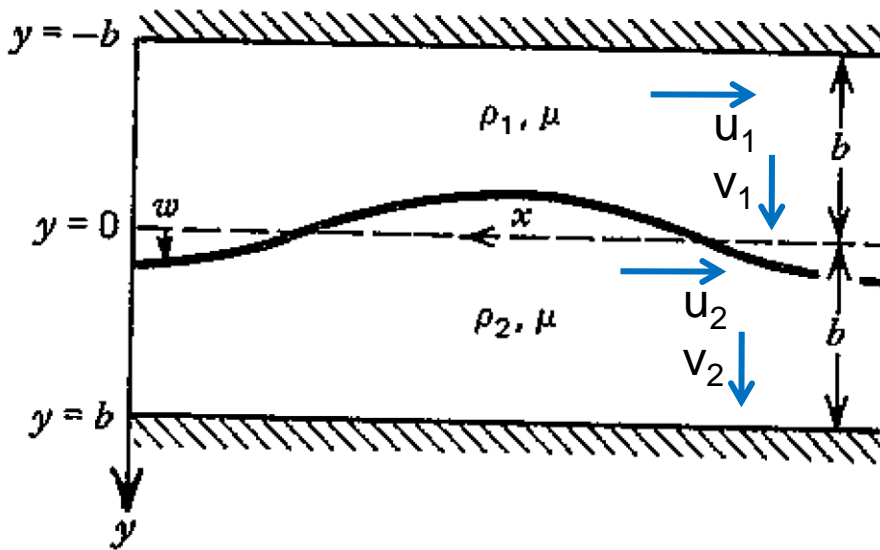
- Boundary conditions:

- $u=v=0$ at $y= -b_1$ and $b_2 \rightarrow u(x,y)$ become

$$u_1(x, -b_1)=0; v_1(x, -b_1)=0$$

$$u_2(x, b_2)=0; v_2(x, b_2)=0$$

6-21 The Rayleigh–Taylor instability of a dense fluid overlying a lighter fluid.



- Boundary conditions:
 - 1) Rigid at top and bottom ($-b_1$ and b_2)—no slip condition (u continuous)
 $\therefore u=v=0$ at $y = -b_1$ and b_2
 - 2) Displacements and velocities and shear stress must be continuous across boundary between media (i.e., at interface, but since w is small, effectively $y=0$ here)

2) velocities and shear stress must be continuous across boundary between media (i.e., at $y=0$ here because w is small)

- $u_1(x,0)=u_2(x,0); v_1(x,0)=v_2(x,0)$

$$\tau_{xy} = \mu\left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}\right) \text{ is same at boundary,}$$

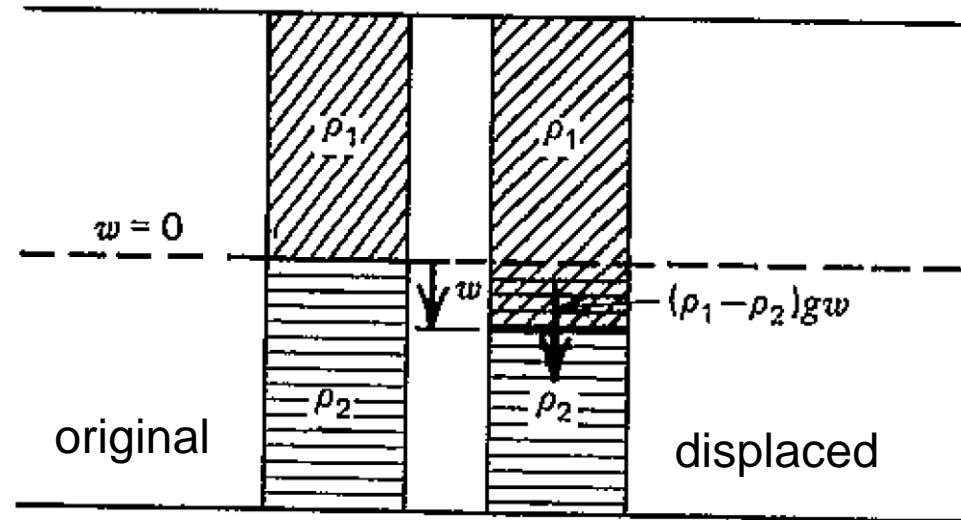
$$\mu\left(\frac{\partial u_1(x,0)}{\partial y} + \frac{\partial v_1(x,0)}{\partial x}\right) = \mu\left(\frac{\partial u_2(x,0)}{\partial y} + \frac{\partial v_2(x,0)}{\partial x}\right)$$

- (x dependence is purely a function of $\sin(2\pi x/\lambda)$)
- Another key—interface is moving with the same velocity as the fluid, so at $y=0$

$$\frac{\partial w}{\partial t} = v(x,0)$$

Finally, balance forces--buoyancy and fluid flow pressure

6-22 The buoyancy force associated with the displacement of the interface.



$$(\rho_1 - \rho_2)gw = (P_2 - P_1) \text{ at } y = 0$$

Buoyancy

Flow pressure found from integrating 6-72

$$\frac{\partial P}{\partial x} = -\mu \left(\frac{\partial^3 \psi}{\partial x^2 \partial y} + \frac{\partial^3 \psi}{\partial y^3} \right)$$

Final solution after much algebra:

• Solution:

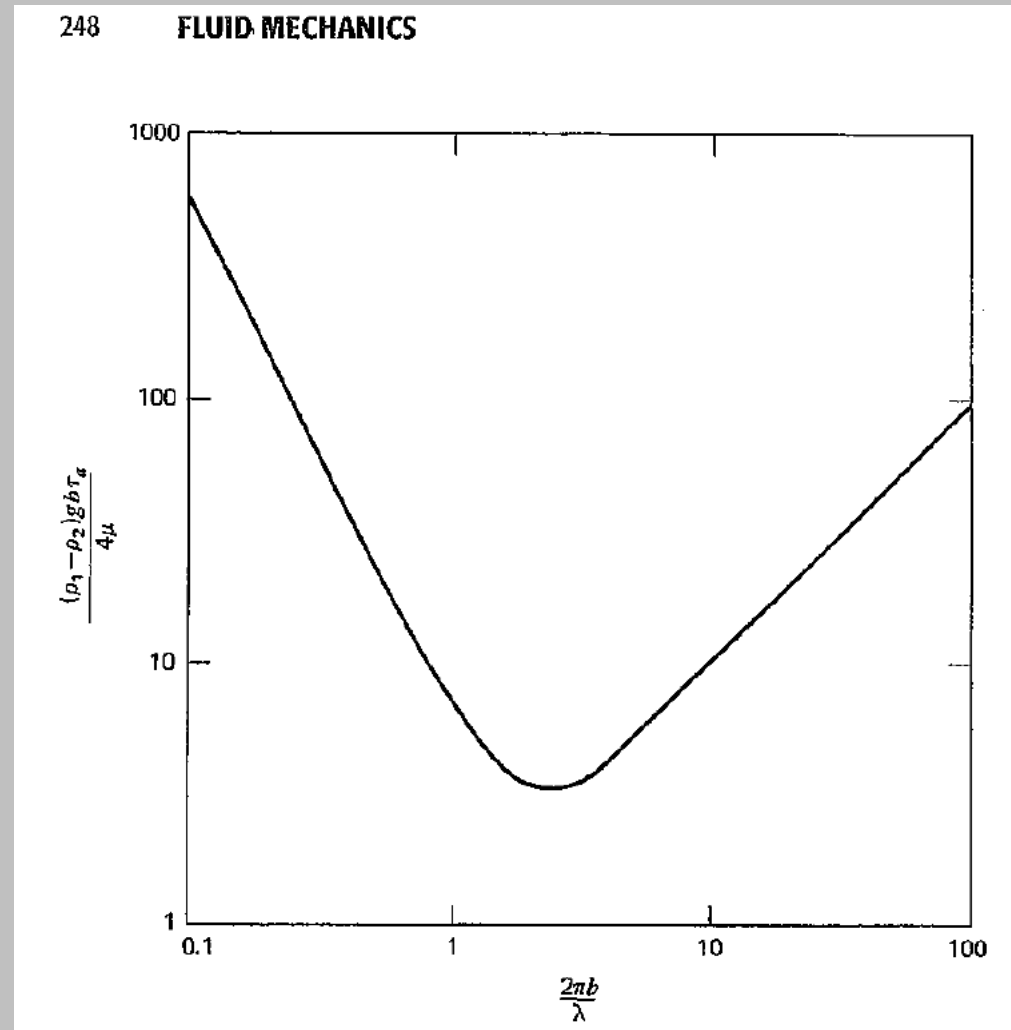
$$w = w_0 e^{t/\tau_a}$$

- Where τ_a is the growth time of the disturbance
- τ_a (Eqn 6-158) is a function of \sinh , $\cosh(2\pi b/\lambda)$ multiplied by

$$\frac{4\mu}{(\rho_2 - \rho_1)gb}$$

- τ_a depends on wavelength, but if have displacements at multiple wavelengths, fastest growing wavelength will dominate (τ_a is a minimum)

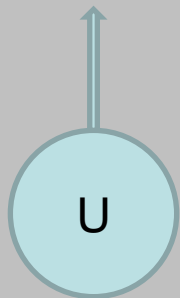
Dimensionless growth time of disturbance



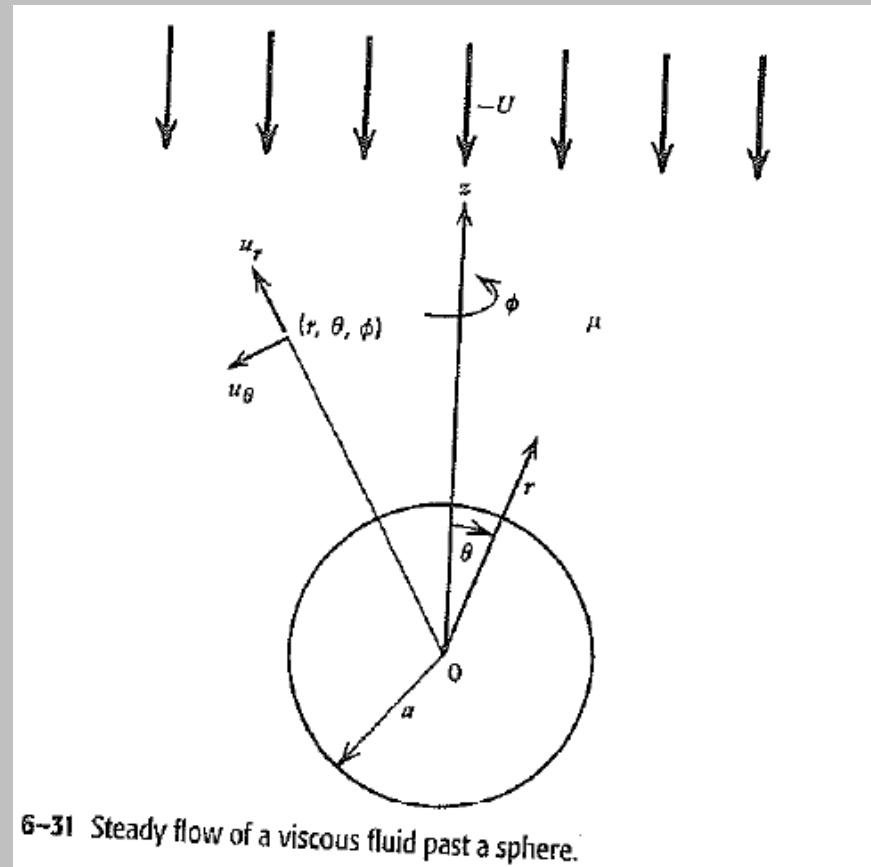
Dimensionless wavenumber

Stokes' Flow: How fast does a body fall due to its own weight?

- Applies in limit of very viscous fluid, with $Re < 1$ (reversible flow)
- Applications:
 - Fall of pieces of slab
 - Rise of plumes/magma
 - Fall of metal probe

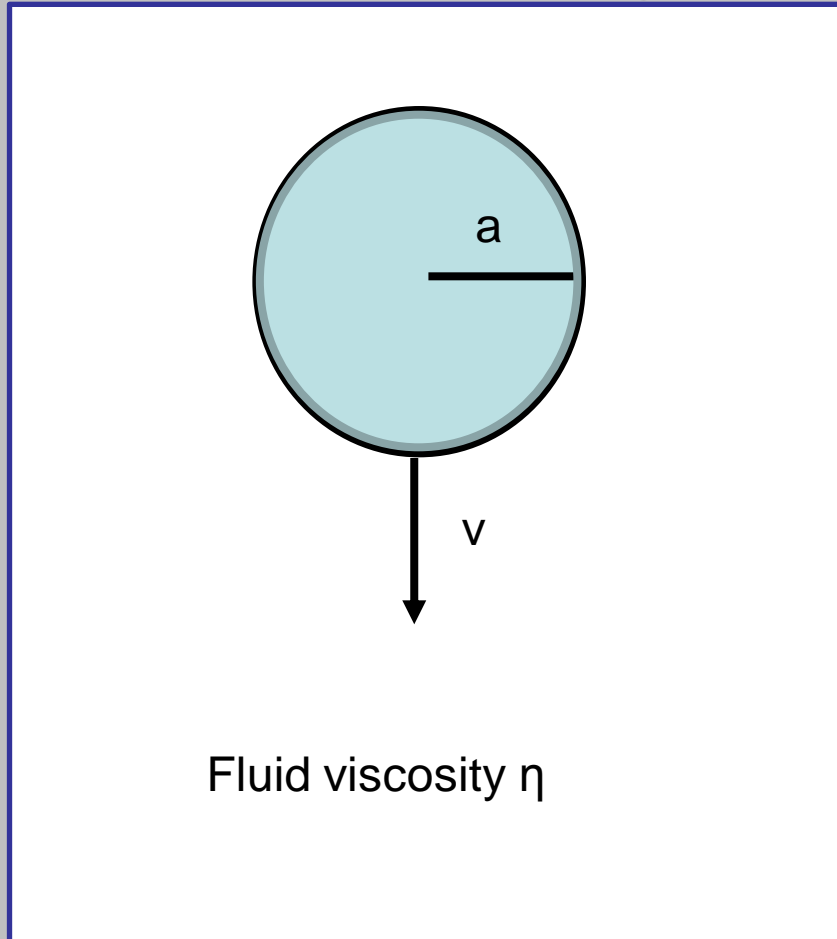


Ball rises through stationary fluid or fluid flows past stationary ball

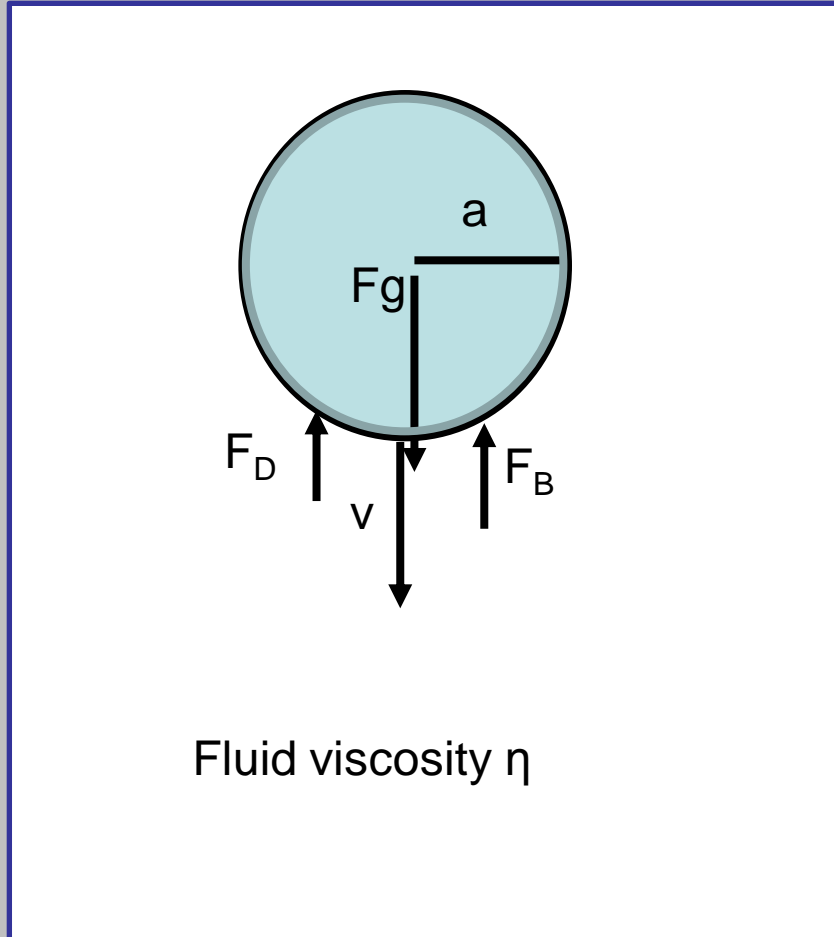


6-31 Steady flow of a viscous fluid past a sphere.

Sphere Falling in a Fluid

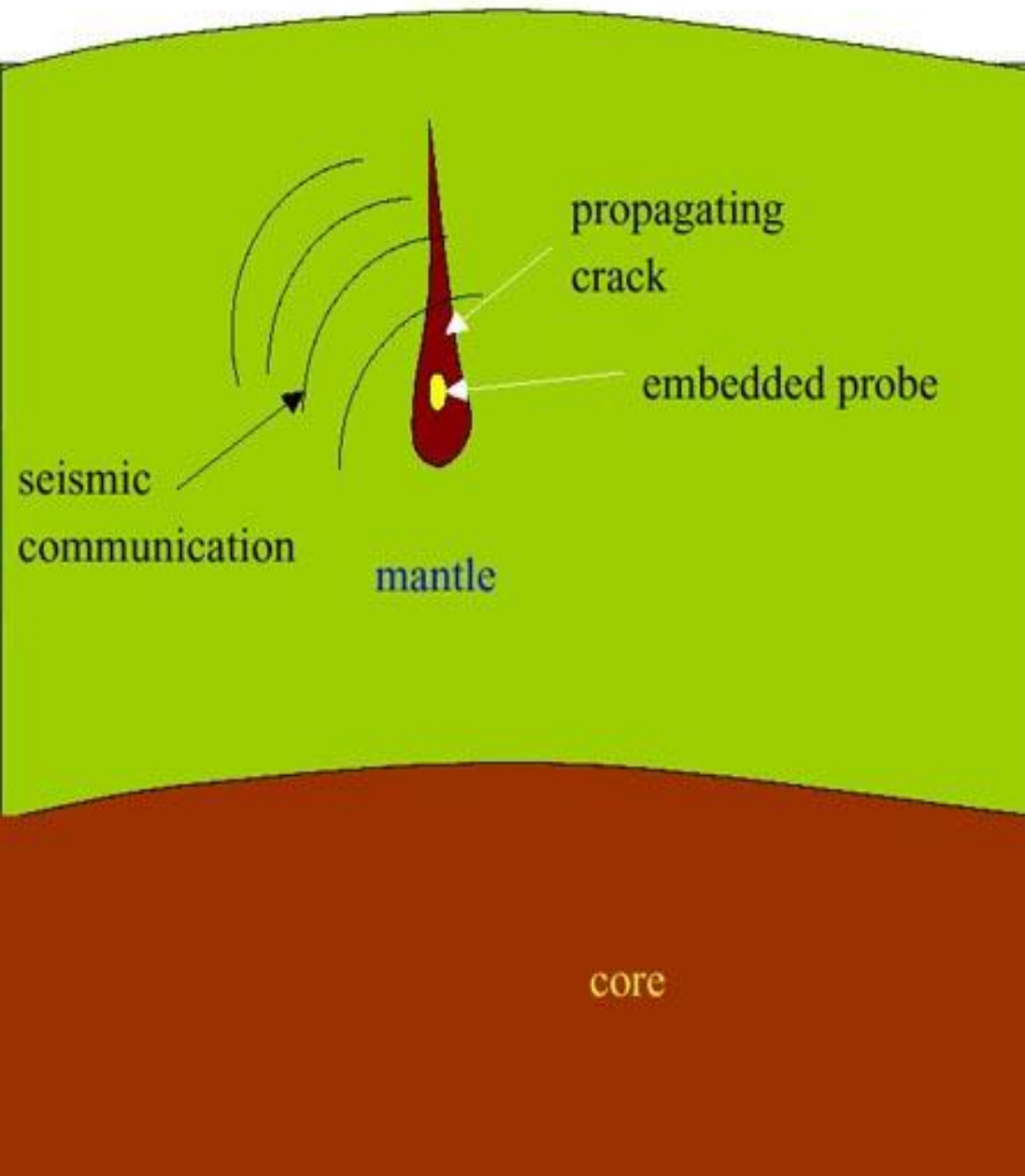


Sphere Falling in a Fluid



$$F_g + F_B + F_D = 0$$

Fall of Iron into Core



Stevenson, David J. Mission to Earth's Core -A Modest Proposal. *Nature*, 423, 239-240, 2003. (in course notes)

About 1 week to get to core

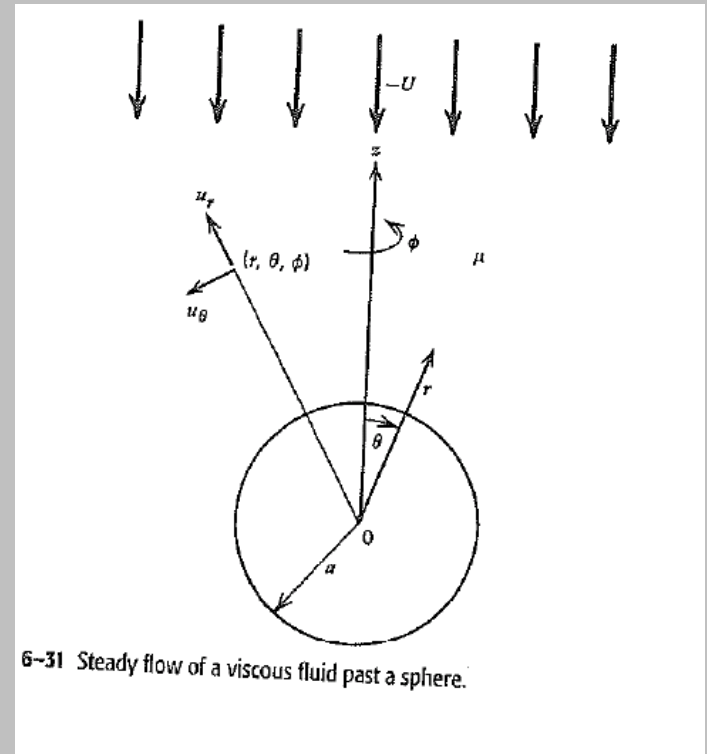
Balance gravity (Buoyancy) and Viscous drag forces

- Dominant equations: continuity equation and pressure equation again, same as before but now geometry and boundary conditions change

$$\vec{\nabla} \cdot \vec{u} = 0 \quad \vec{\nabla} P = \mu \nabla^2 u$$

- Where $P = p - \rho_f g y$
- $\rho_f =$ density of fluid
- $\rho_s =$ density of sphere

$$\text{Re} = \frac{\rho_f U (2a)}{\mu}$$



Boundary Conditions

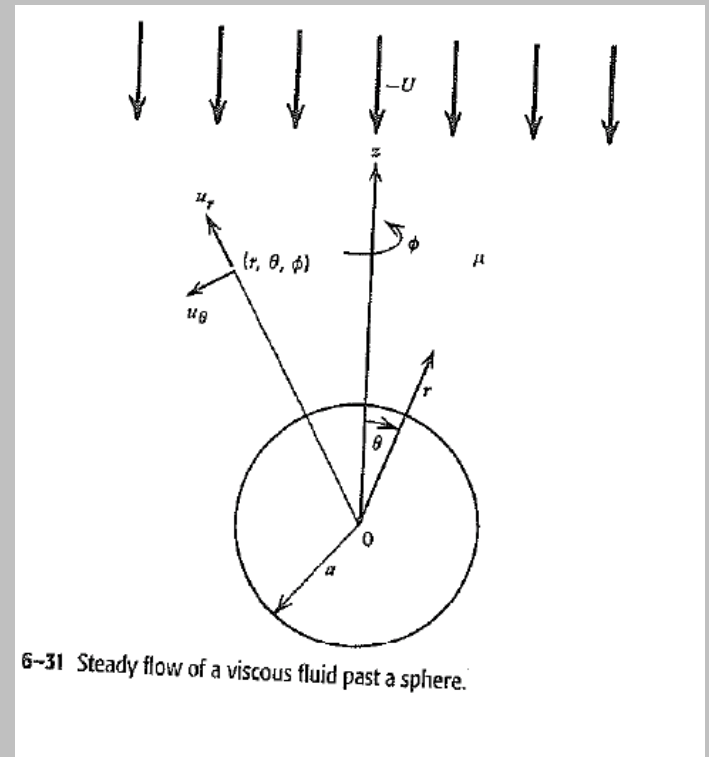
- As $r \rightarrow \infty$

$u_r \rightarrow -U$ in z direction

$u_r \rightarrow -U \cos \theta$ $u_\theta \rightarrow U \sin \theta$

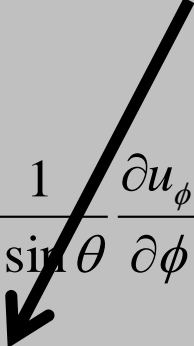
No-slip on sphere: at $r=a$

$$u_r = u_\theta = 0$$



Spherical Coordinates:

Continuity equation becomes:

$$0 = \vec{\nabla} \cdot \vec{u} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 u_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (u_\theta \sin \theta) + \left(\frac{1}{r \sin \theta} \frac{\partial u_\phi}{\partial \phi} \right)$$


But since $u_\phi=0$, last term is 0

To solve equation, also need the Laplacian of u:

$$\nabla^2 \vec{u} = \vec{\nabla}(\vec{\nabla} \cdot \vec{u}) - \vec{\nabla} \times (\vec{\nabla} \times \vec{u})$$

$$\vec{\nabla} \times \vec{u} = \frac{1}{r \sin \theta} \left[\frac{\partial}{\partial \theta} (u_\phi \sin \theta) - \frac{\partial u_\theta}{\partial \phi} \right] \hat{r} + \frac{1}{r} \left[\frac{1}{\sin \theta} \frac{\partial u_r}{\partial \phi} - \frac{\partial (r u_\theta)}{\partial r} \right] \hat{\theta} + \frac{1}{r} \left[\frac{\partial (r u_\theta)}{\partial r} - \frac{\partial u_r}{\partial \theta} \right] \hat{\phi}$$

Pressure forces: Terms in P

Viscous forces: Terms in $\mu \nabla^2 u$

Solution

- Surprisingly, most terms drop out and ...
- Pressure due to fluid flow is (Eq 6-216):

$$p = \frac{3\mu a U}{2r^2} \cos \theta$$

- Integrate to get downward “drag” (force) due to fluid pressure across sphere:

$$D_p = 2\pi\mu a U$$

Viscous drag:

- Using 3-D formulation of stress again:

$$\vec{\tau} = \mu(\vec{\nabla}\vec{u} + \vec{\nabla}\vec{u}^T)$$

Integrate to get Viscous Drag $D_v = 4\pi\mu aU$

So total Drag $F_D = \text{Viscous Drag} + \text{Pressure}$

$$\text{Drag} = D_p + D_v = 6\pi\mu aU$$

Speed of rise or fall:

- Balance Buoyancy Forces with Drag forces for steady-state case (no acceleration):
- $F_B = (\rho_f - \rho_s)g \frac{4\pi a^3}{3} = F_D = 6\pi\mu aU$
- Solve for U
- For faster flow, $Re > 1$, more difficult: use dimensionless drag coefficient C_D

$$C_D \equiv \frac{F_D}{\frac{1}{2}\rho_f U^2 \pi a^2} = \frac{24}{Re} \quad (6-226)$$

Pressure due to vel.

Sphere x-sec area (shadow)

- Stokes flow:

$$U = \frac{2(\rho_f - \rho_s)ga^2}{9\mu} \quad (6-229)$$

- $Re > 1$:

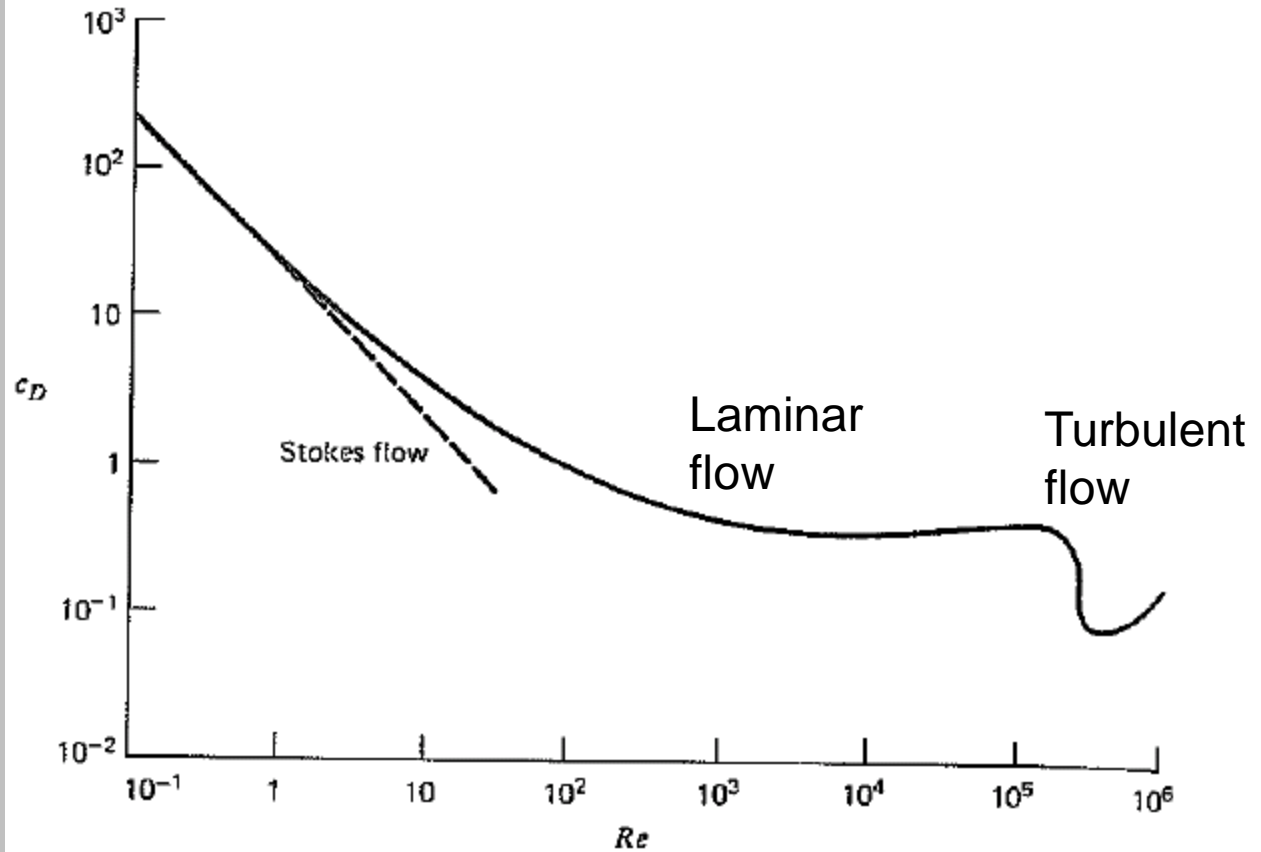
$$U = \left[\frac{8(\rho_f - \rho_s)ga}{3C_D\rho_f} \right]^{1/2} \quad (6-230)$$

$$C_D \equiv \frac{F_D}{\frac{1}{2}\rho_f U^2 \pi a^2} = \frac{24}{Re} \quad (6-226)$$

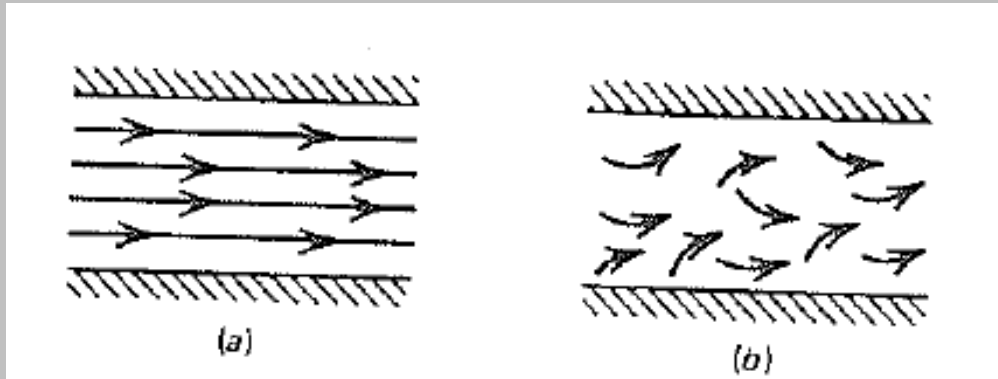
\bar{u} = avg speed

$$Re = \frac{\rho \bar{u} D}{\mu} = \frac{\bar{u} D}{\nu}$$

Note—units work out in both cases



Compare to pipe flow:



laminar

turbulent

Depends on dimensionless variables: Friction factor f and Reynolds number Re

$$f \equiv \frac{-4R}{\rho \bar{u}^2} \frac{dp}{dx}$$

6-7 Dependence of the friction factor f on the Reynolds number Re for laminar flow, from Equation (6-41), and for turbulent flow, from Equation (6-42).

